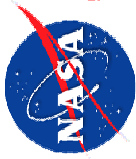


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Electrical Arc Ignition Testing of Spacesuit Materials

October 2006

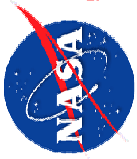
Sarah Smith
Tim Gallus
Susana Tapia
Elizabeth Ball
Harold Beeson



Background

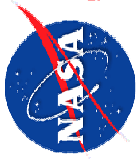
- Testing in response to frayed cable discovered during spacewalk
- Reliance on Apollo-era arc testing
 - Limited applicability to current materials
 - Significant changes in voltage and circuitry
 - Poor understanding of test configuration





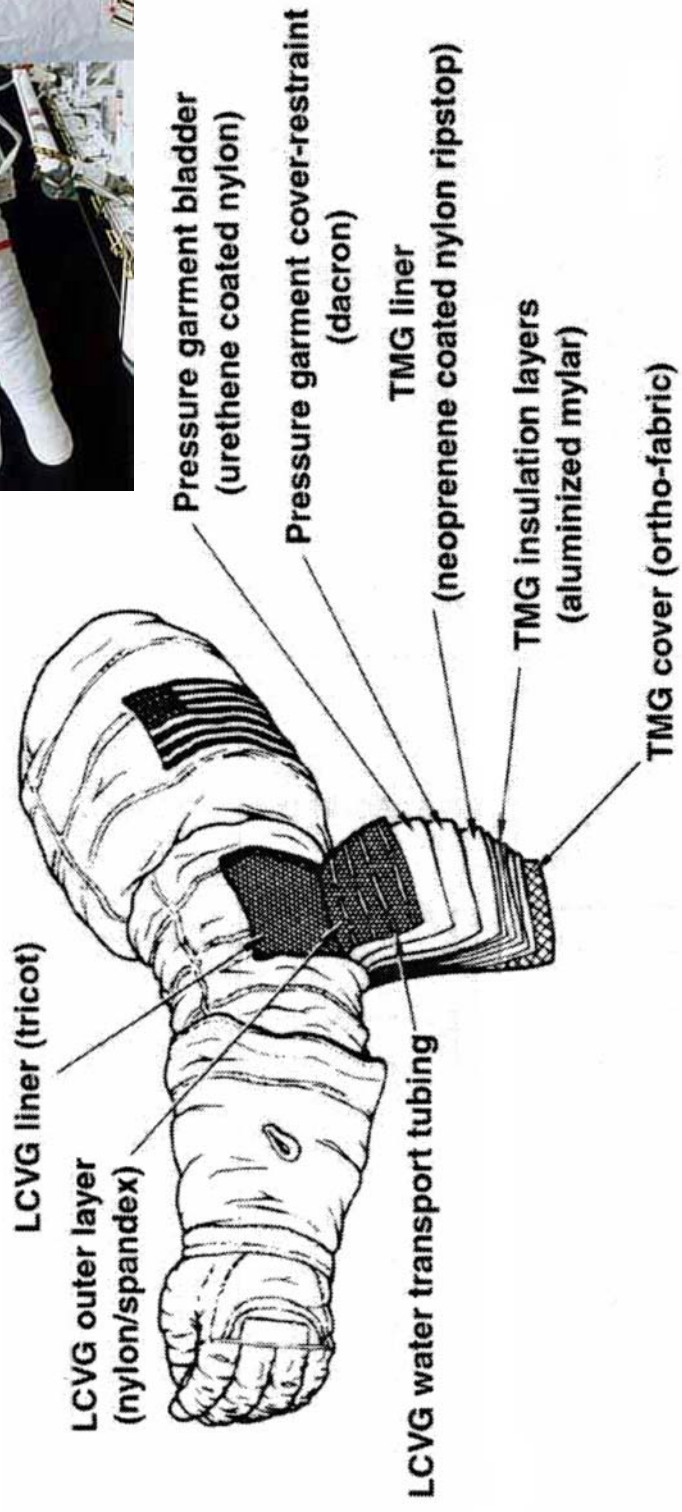
Test Objectives

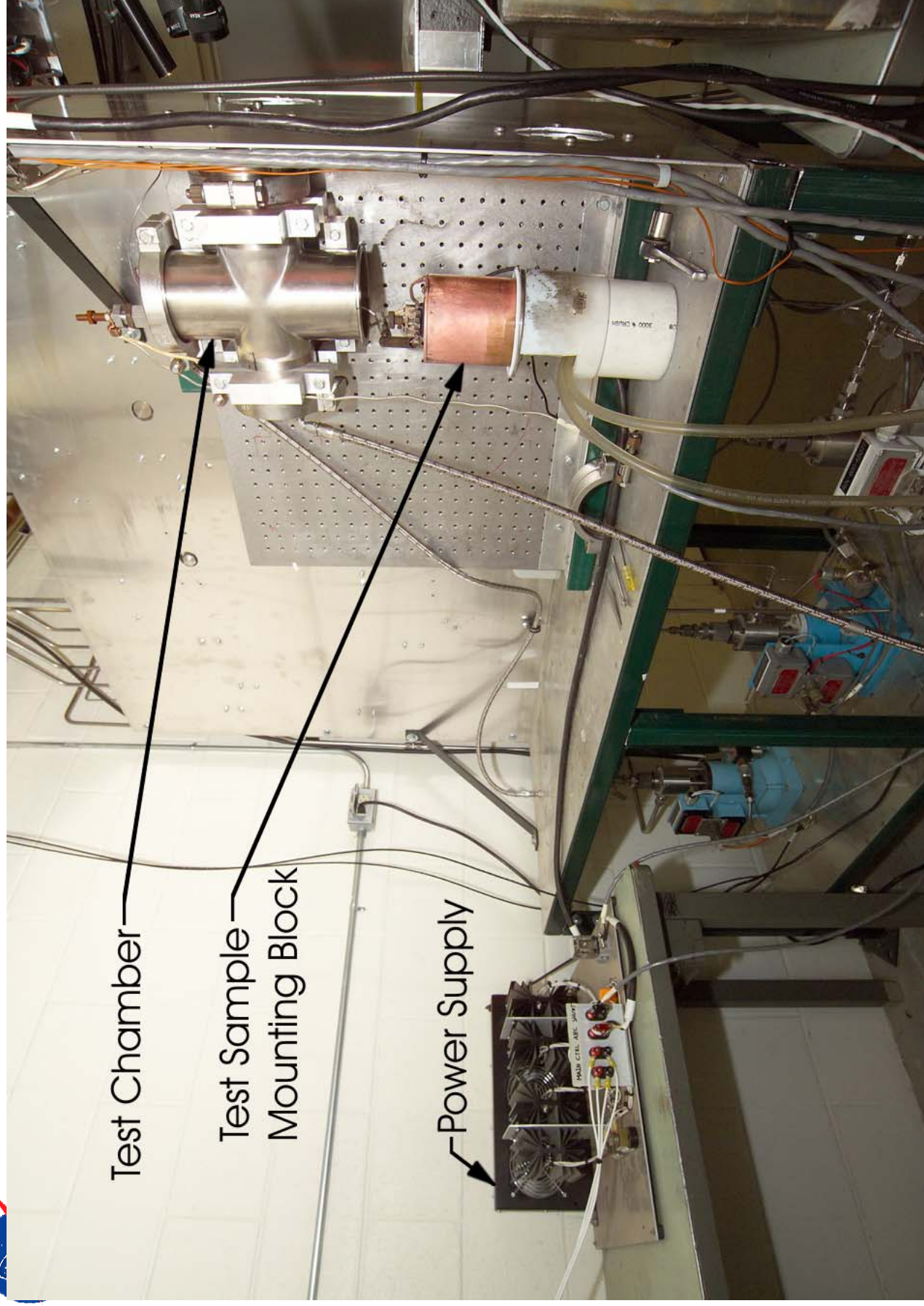
- Gain better understanding of Apollo-era data
- Investigate new test methods
- Characterize minimum current levels necessary for combustion of EMU materials (at a given voltage)



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Test Sample Materials





Test Chamber

Test Sample
Mounting Block

Power Supply



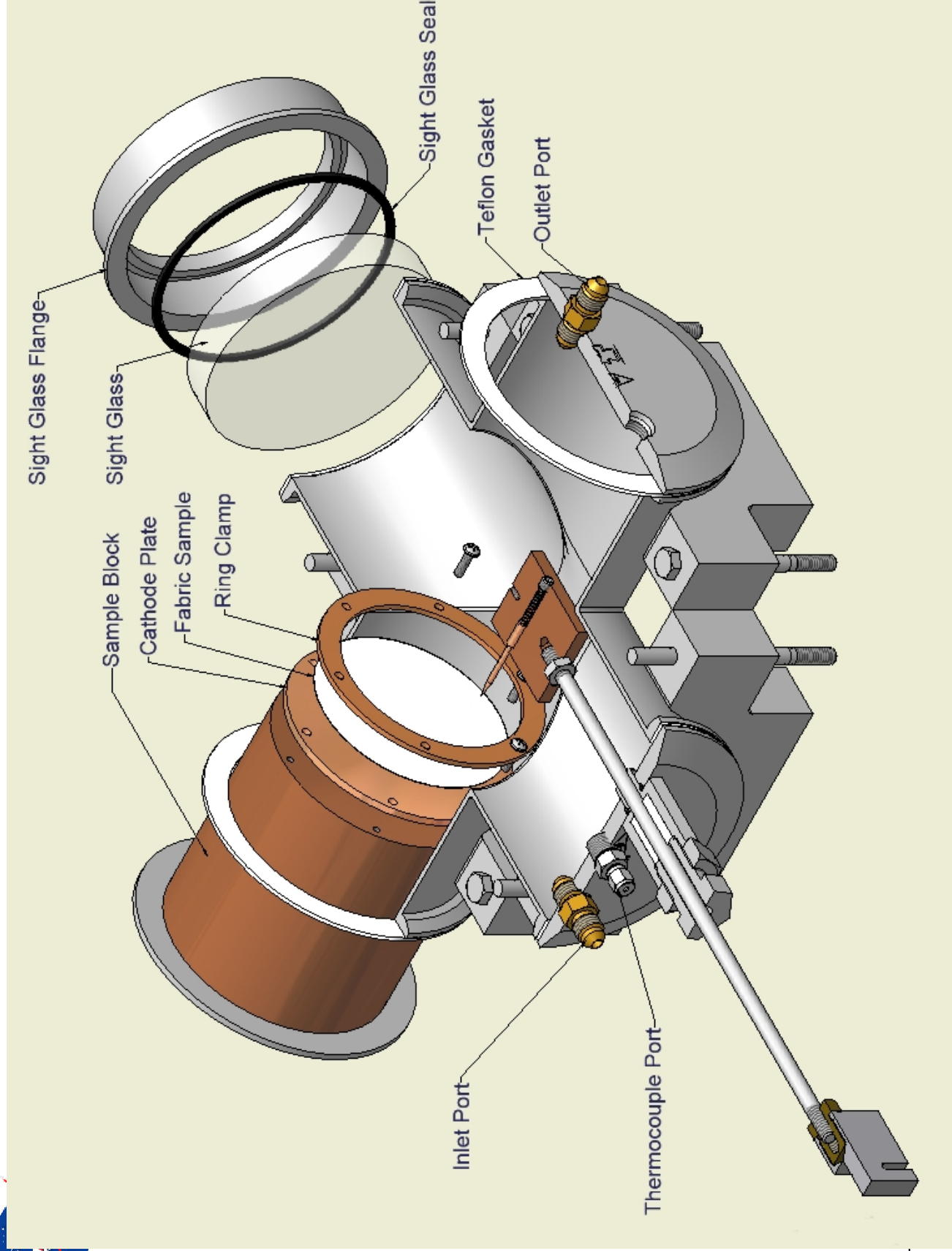
Test Methods

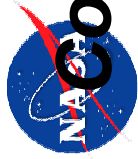
- [Multiple location intermittent arcing \(scratch\) test](#)
- [Single location intermittent arcing \(poke\) test](#)
- [Single location wire-break arcing test](#)



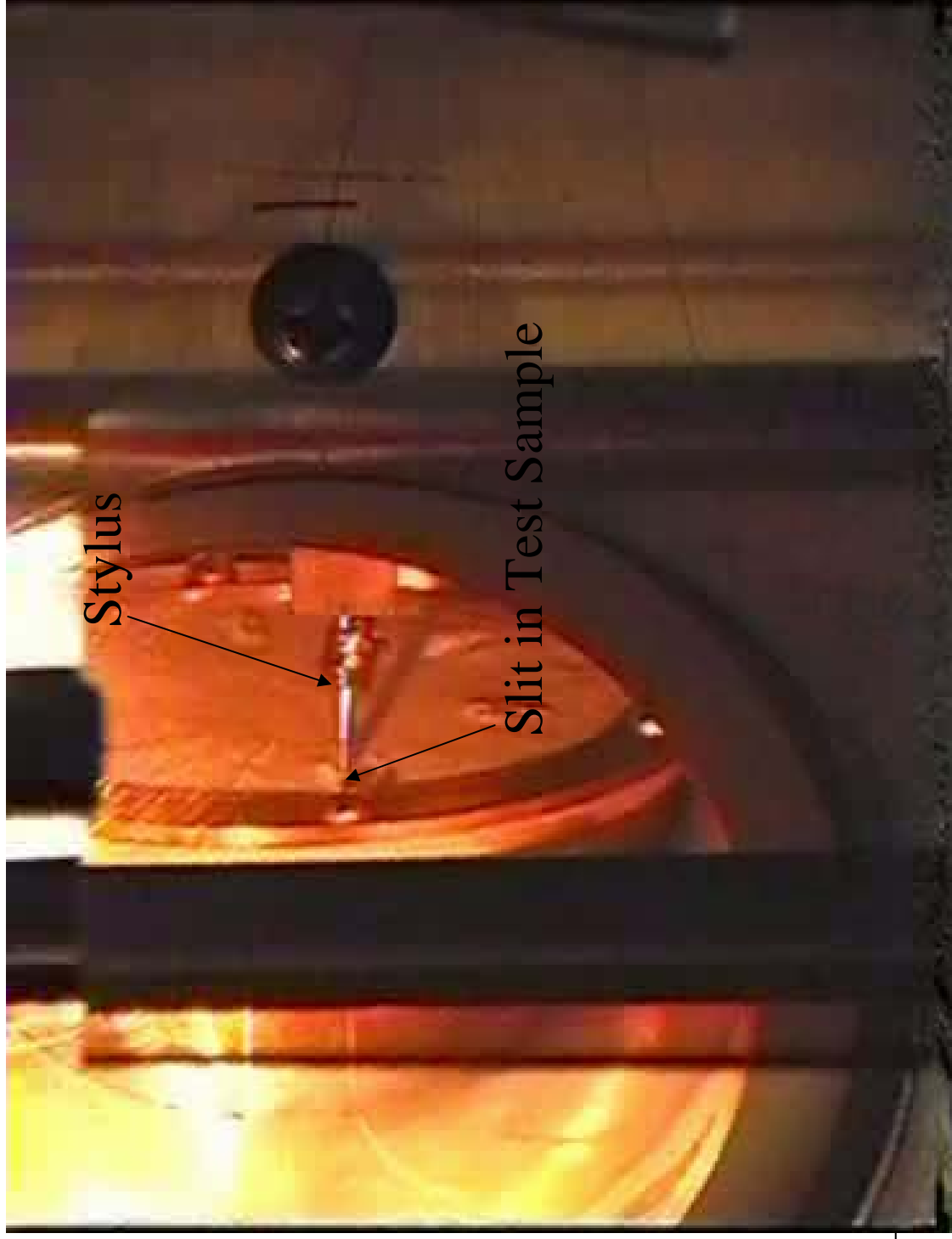
Scratch Test Objectives

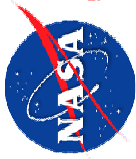
- Simulate Apollo-era testing
- Determine configurational effects
- Test materials currently used in the EMU





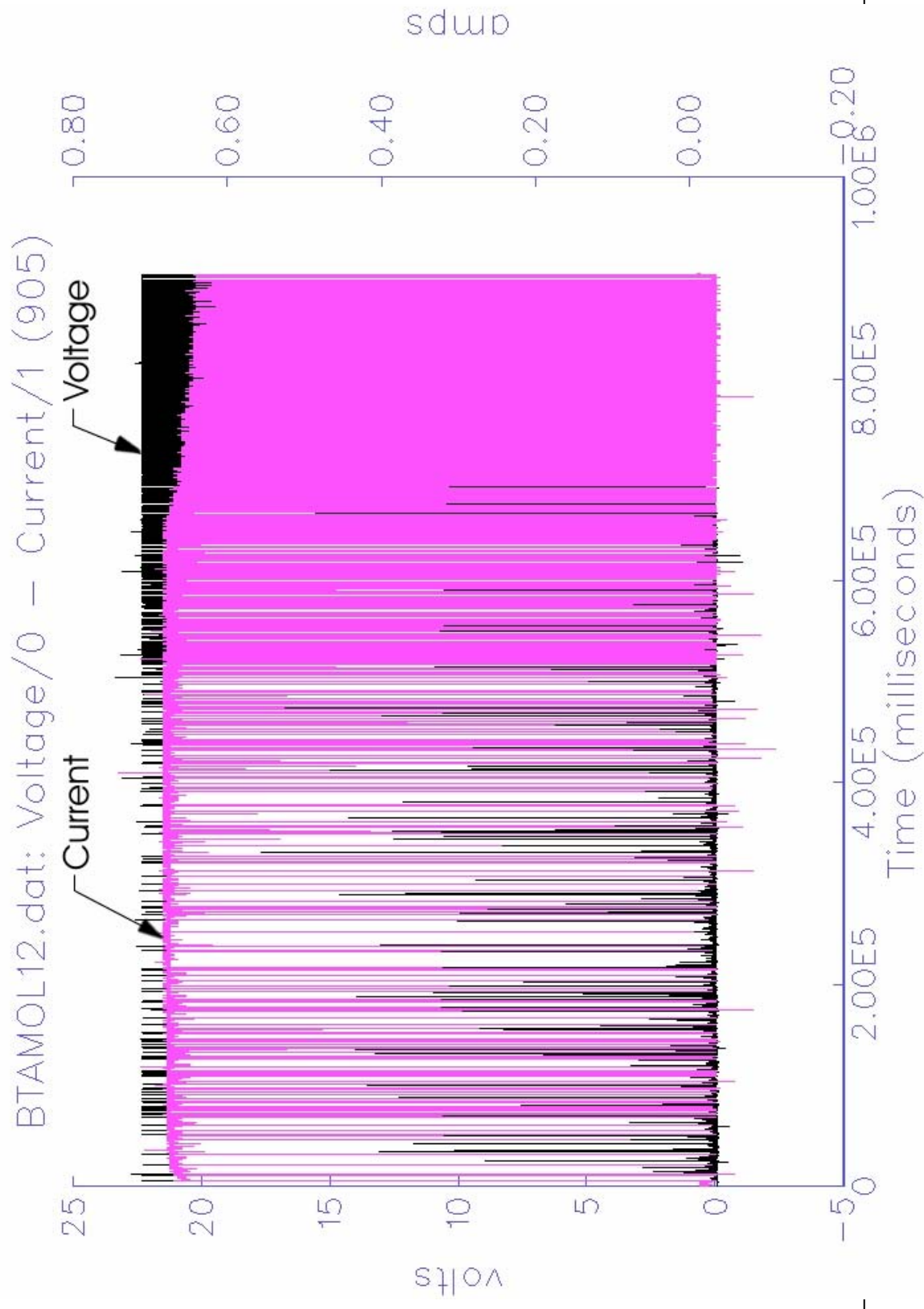
Cotton Scratch Test Video

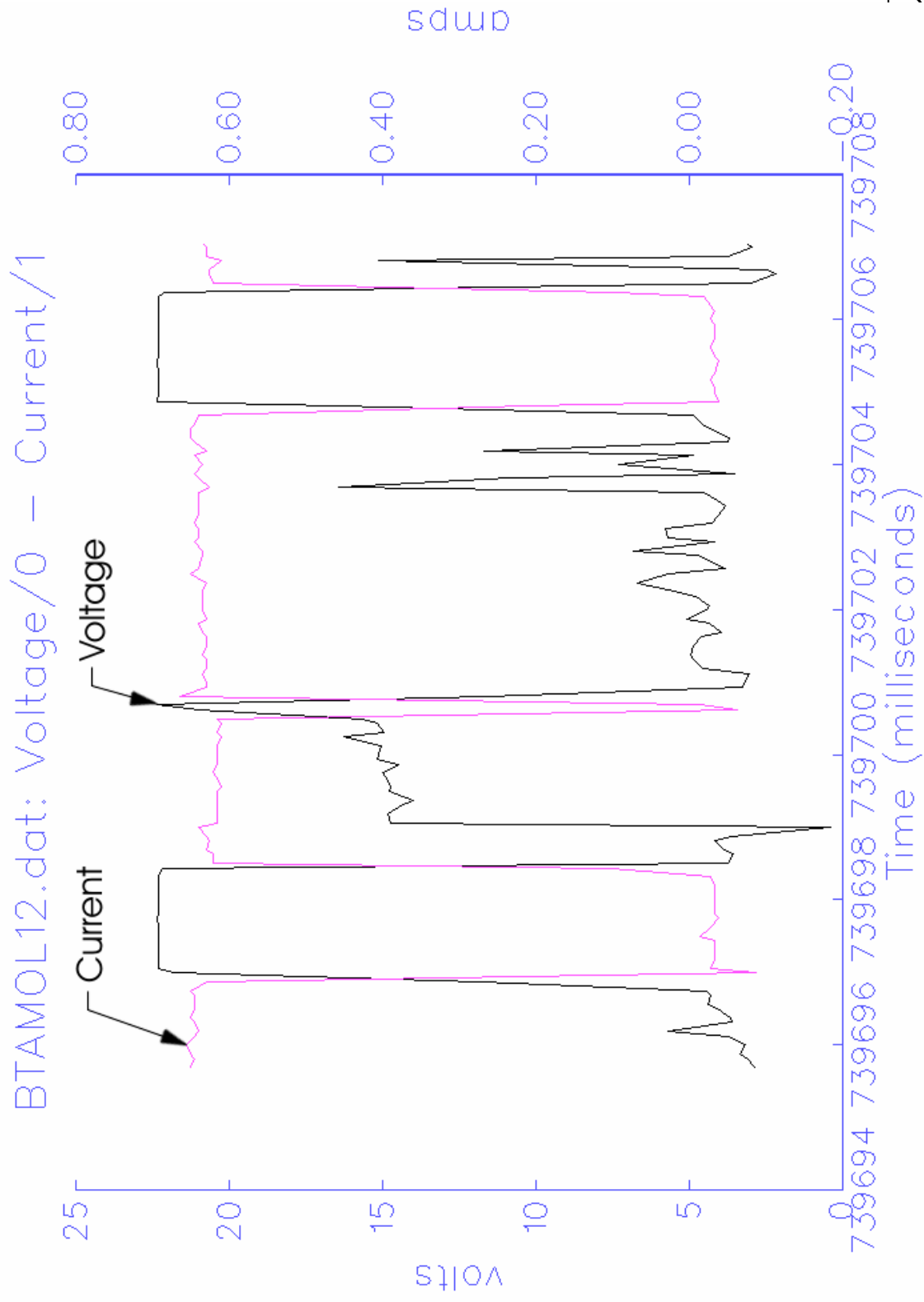


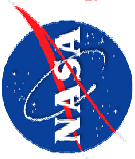


Scratch Test Results

- Testing yielded results similar to Apollo-era testing
- Frayed materials more reactive
- No distinguishable difference between horizontal samples and vertical samples
- Tests performed at 23.5 psia 100% O₂, 22.5 V
 - 7 materials tested
 - Current required for ignition ranged from 0.8 A to 1.4 A







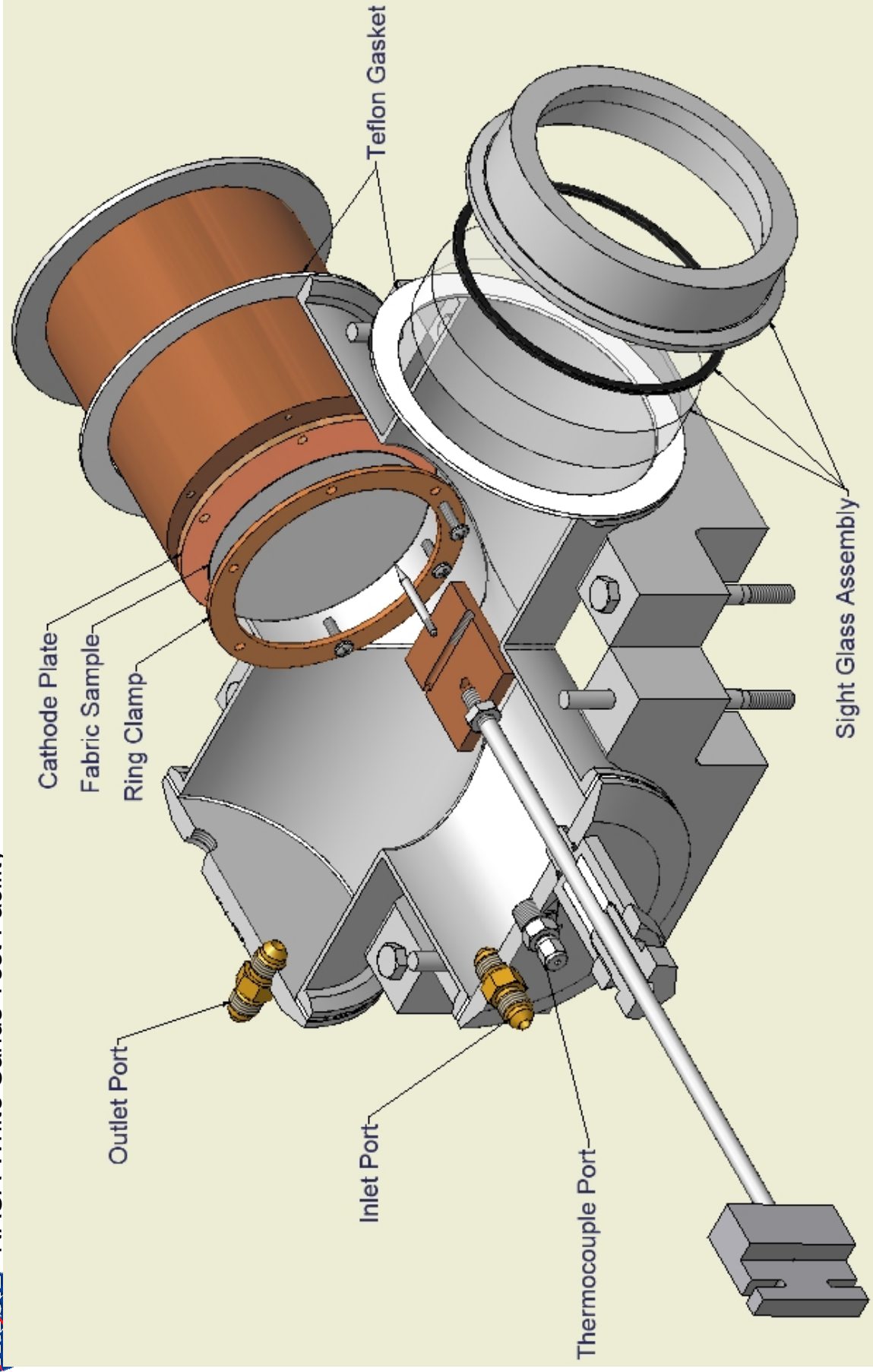
Scratch Test Problems

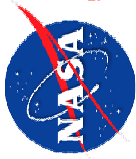
- Not possible to determine which arc ignited material
- Arc energies vary widely from test to test and arc to arc
- Difficult to ensure that test sample material is in intimate contact with arcing event
- Configuration not realistic for inside spacesuit because of size of stylus



Poke Test Objectives

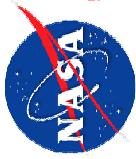
- Determine whether more severe to arc with wires or stylus
- Determine whether more severe to arc in single location (poke test) or multiple locations (scratch test)





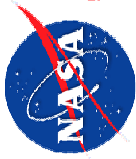
Poke Test Results

- Poke test results consistent with scratch test results
 - No detectable difference between arcing in one location or multiple locations
- Tests showed that it is more severe to arc with a wire than a stylus
 - Wires are flammable and can burn in oxygen
 - Burning wires easily ignite test materials



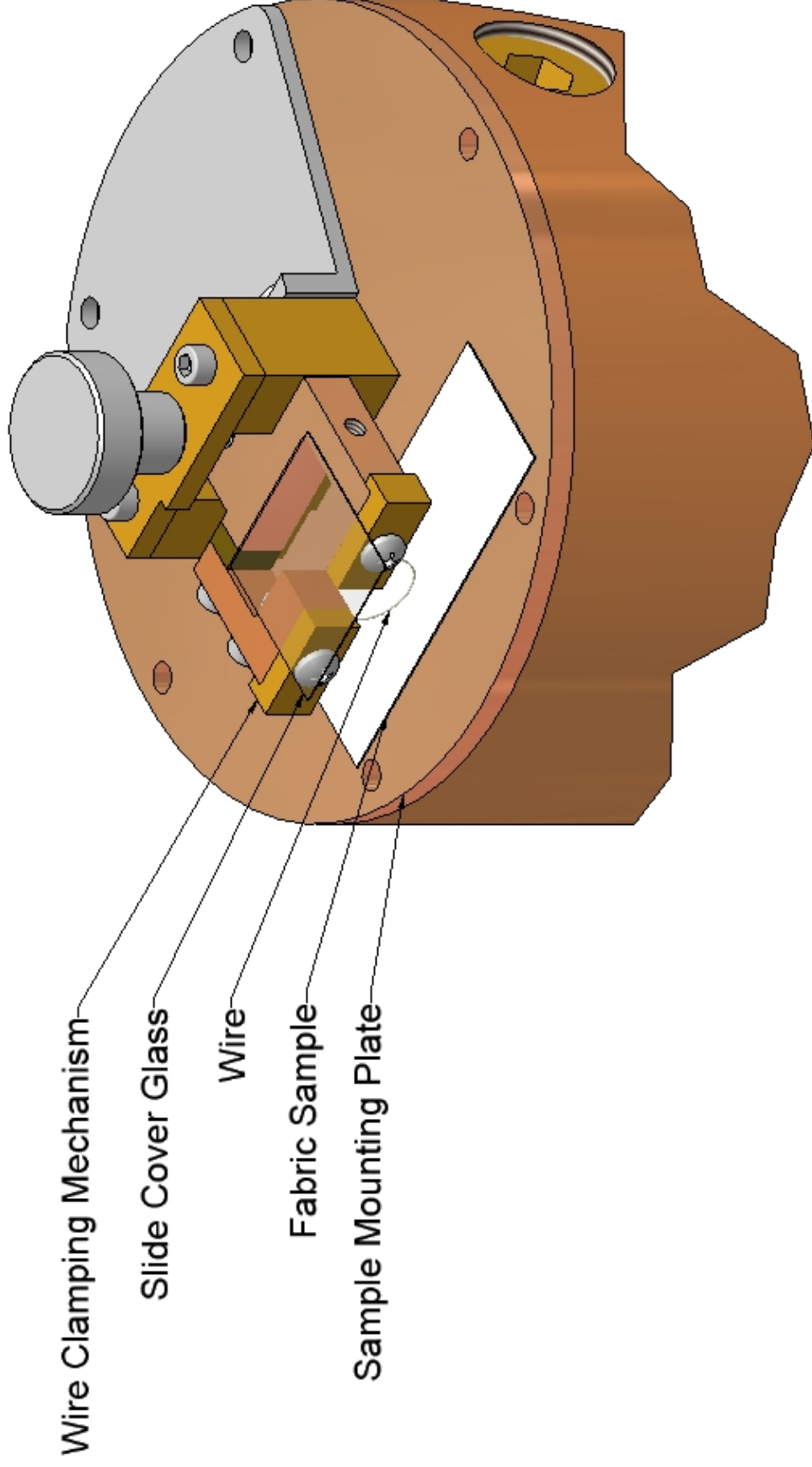
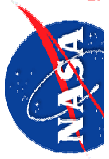
Poke Test Problems

- Not possible to determine which arc ignited material
- Arc energies vary widely from test to test and arc to arc
- Difficult to ensure that test sample material is in intimate contact with arcing event

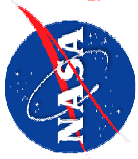


Wire-break Test Objectives

- Reduce variability in tests
- Test all materials
- Determine whether ignition is dependent on voltage or current



| AWG Size | Diameter (in.) | % of Flight Wire Cross Sectional Area | Approximate Current Required to Break Wire (A) |
|----------|----------------|--|--|
| 34 | 0.0063 | 1550 | 9.00 |
| 38 | 0.004 | 625 | 5.00 |
| 39 | 0.0035 | 479 | 3.80 |
| 40 | 0.0031 | 375 | 3.00 |
| 41 | 0.0028 | 306 | 2.60 |
| 42 | 0.0025 | 244 | 2.30 |
| 43 | 0.0022 | 189 | 1.80 |
| 44 | 0.002 | 156 | 1.50 |
| 45 | 0.0018 | 127 | 1.30 |
| 46 | 0.0016 | 100 | 1.10 |
| 47 | 0.0014 | 77 | 0.90 |
| 48 | 0.0012 | 56 | 0.83 |
| 49 | 0.0011 | 47 | 0.70 |
| 50 | 0.001 | 39 | 0.63 |
| 51 | 0.00088 | 30 | 0.50 |
| 52 | 0.00078 | 24 | 0.45 |
| 54 | 0.00062 | 15 | 0.35 |



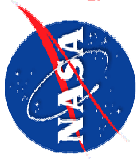
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Cotton Wire-Break Test Video

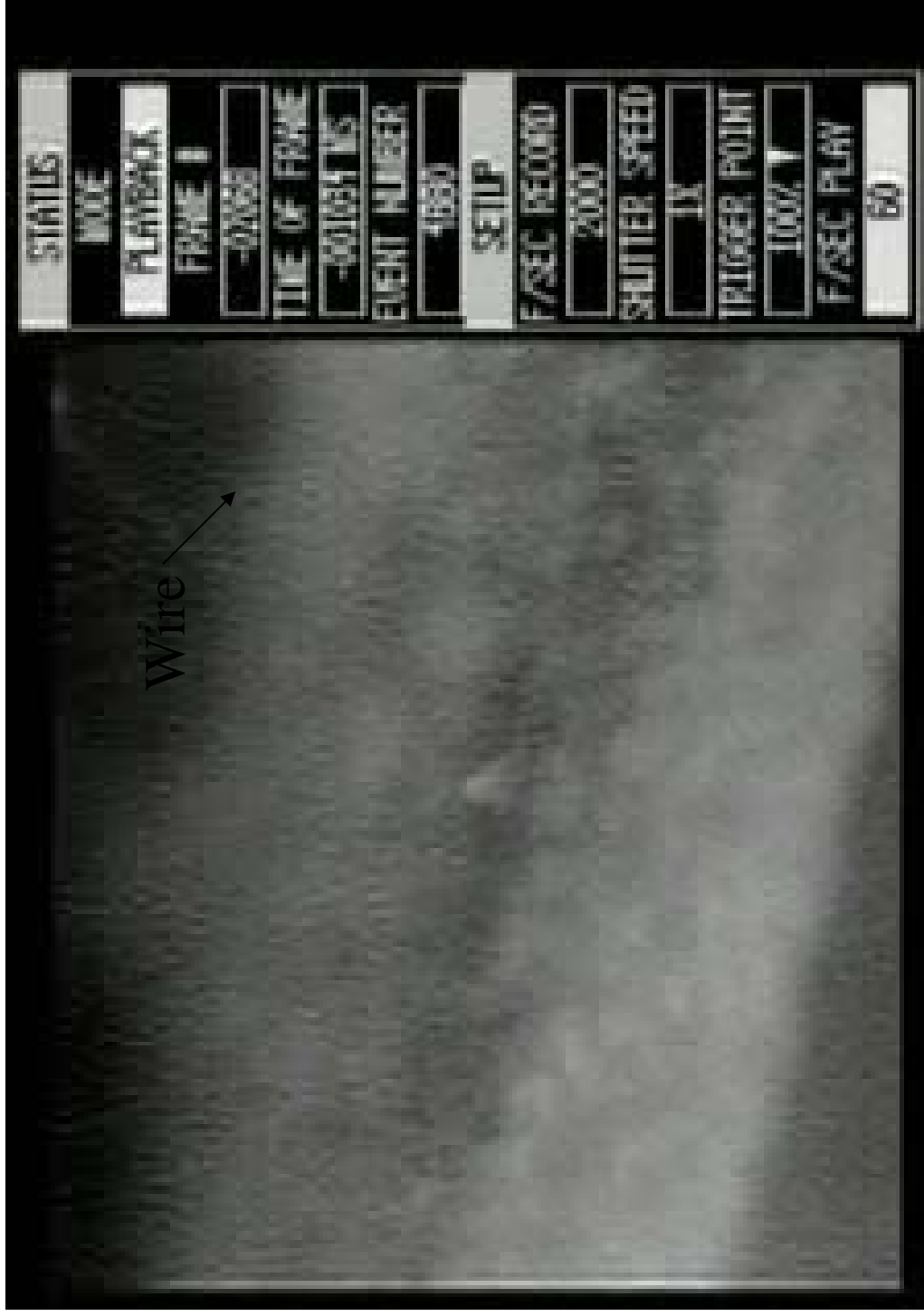


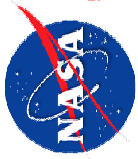
21

21

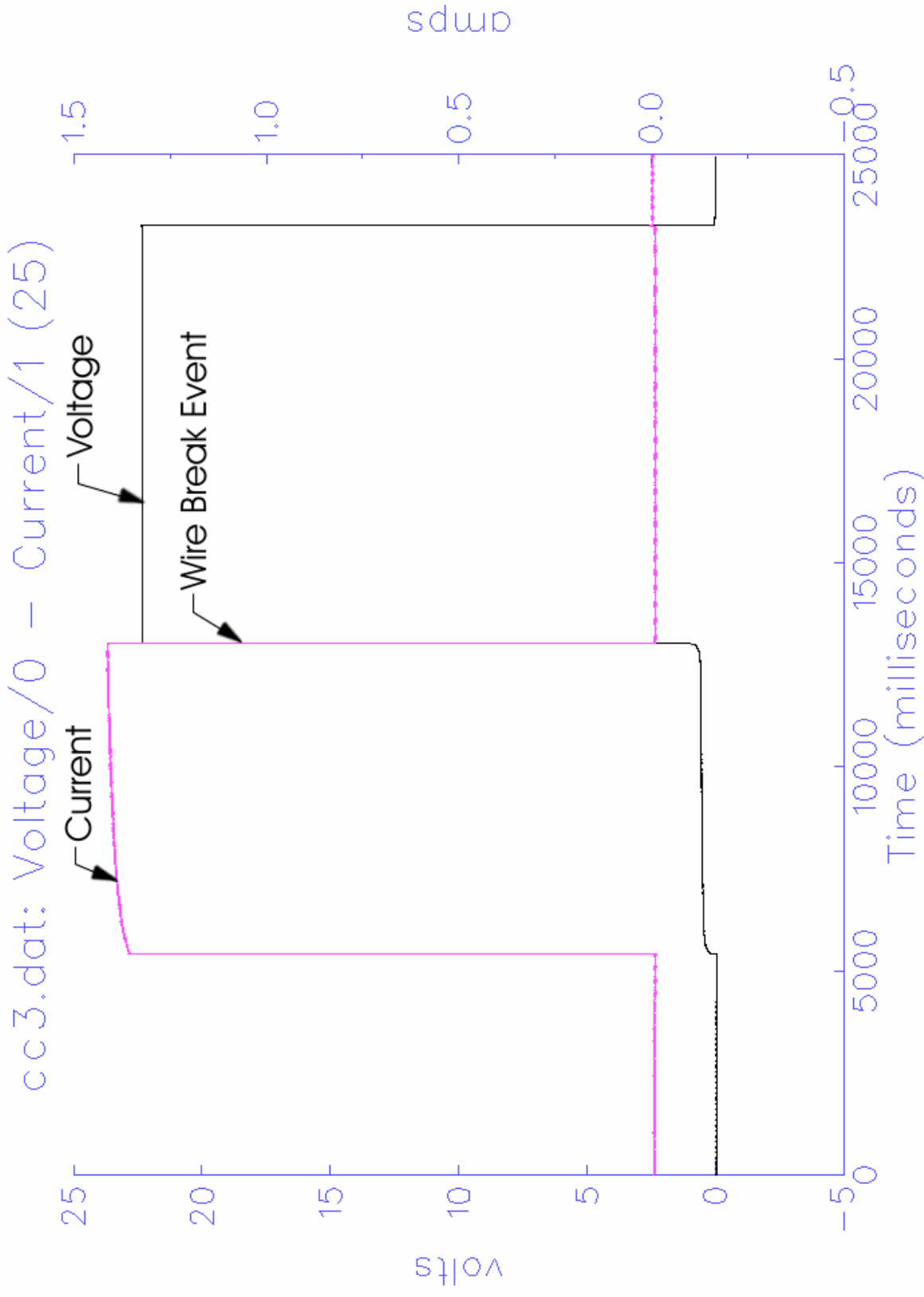


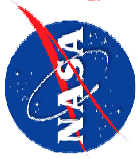
High Speed Cotton Wire-break Test Video





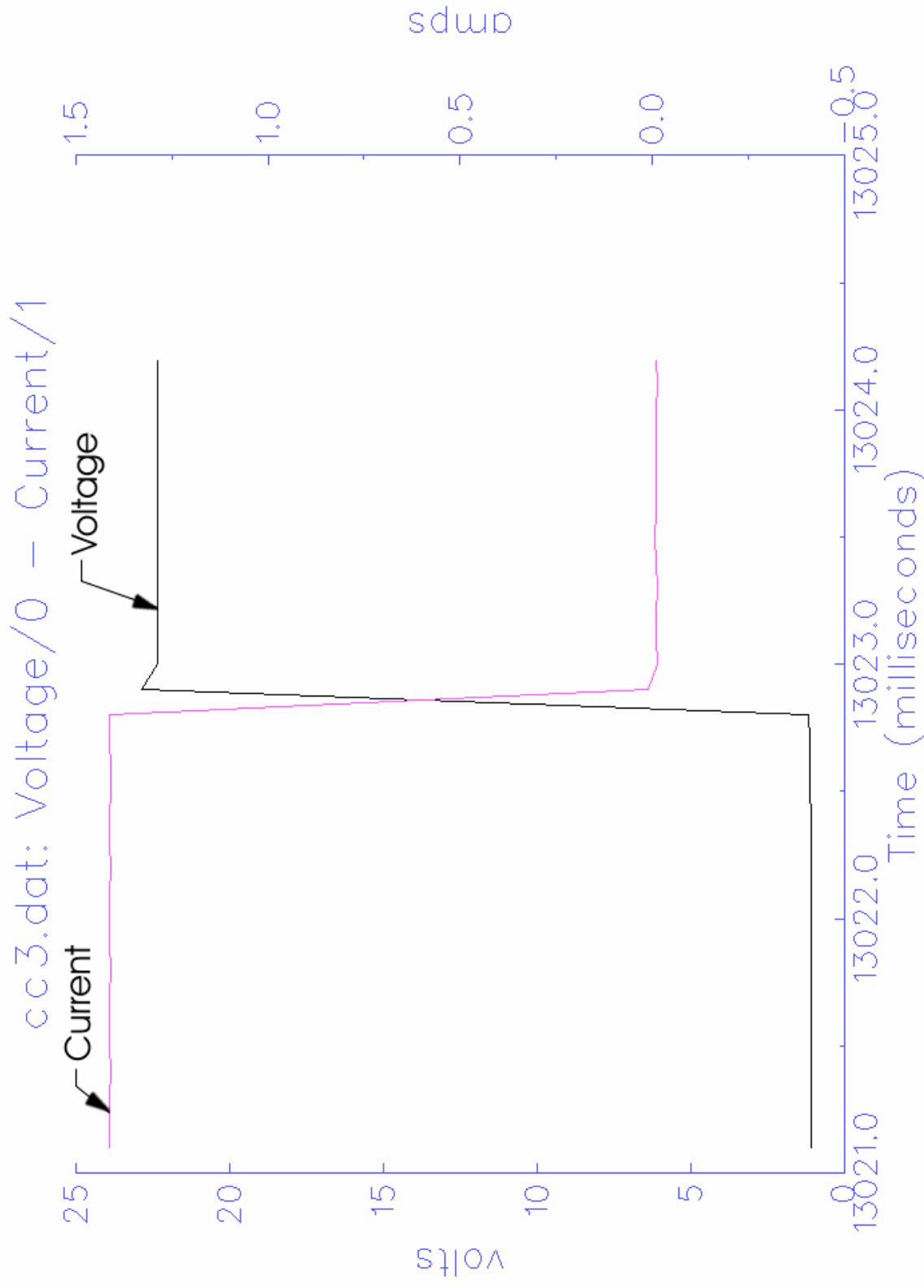
Typical Data Plot





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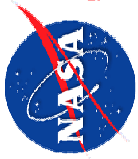
Closeup Data Plot





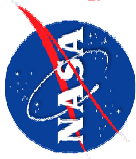
Wire-break Test Results

- Much more severe than scratch and poke tests
- Test conditions
 - 23.5 psia 100% O₂, 22.5 V
 - 50 psia 50% O₂ and 50% N₂, 15 V
- Several materials failed testing at the lowest possible current, ~0.3 A
- Current required for ignition for most materials ranged from <0.3 A to 0.97 A



Wire-Break Test Results (cont.)

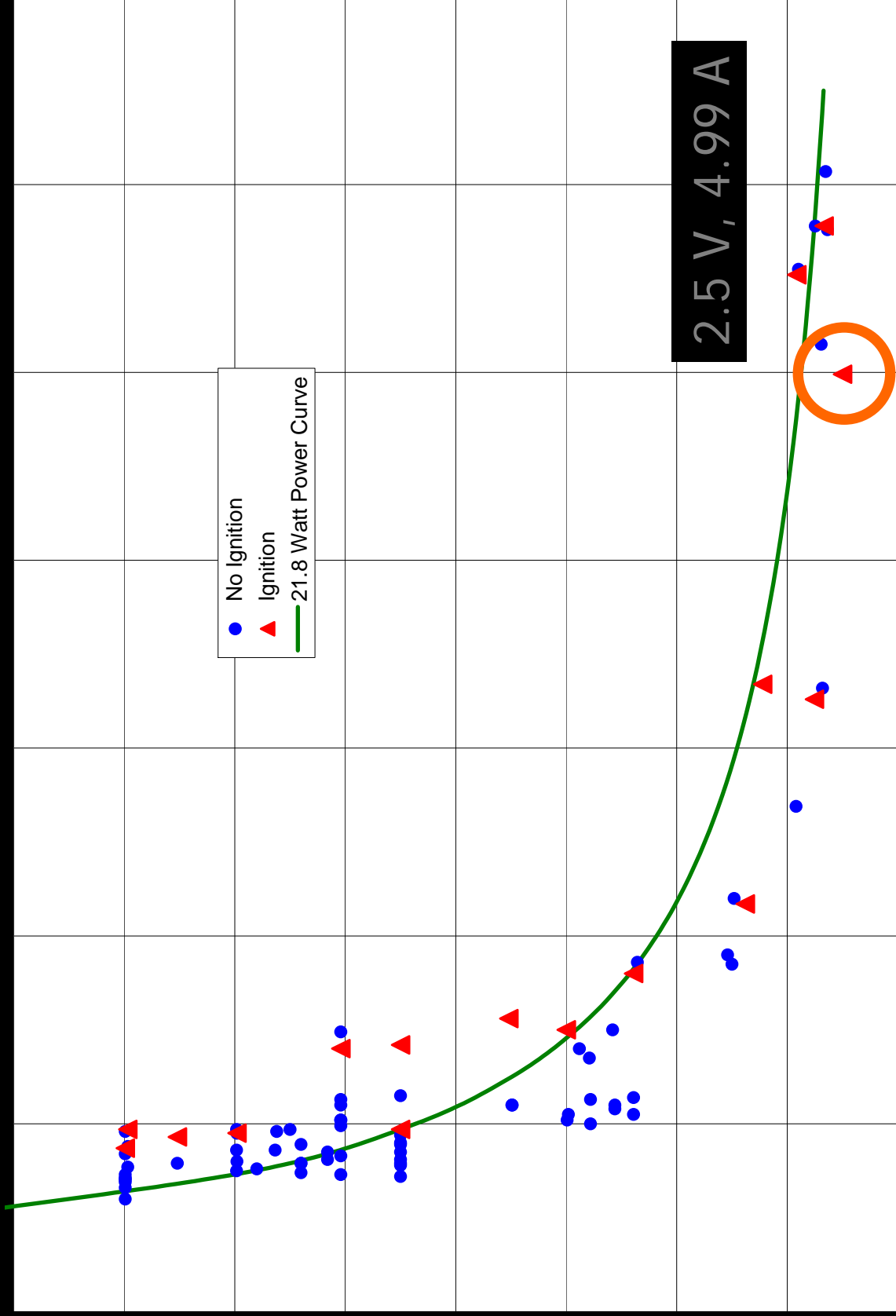
- Gore-Tex only ignited under much more severe conditions
 - 100% O₂, 54 psia
 - Zigzag wire configuration

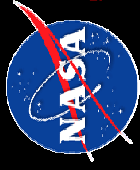


Wire-break Tests vs. Scratch Tests

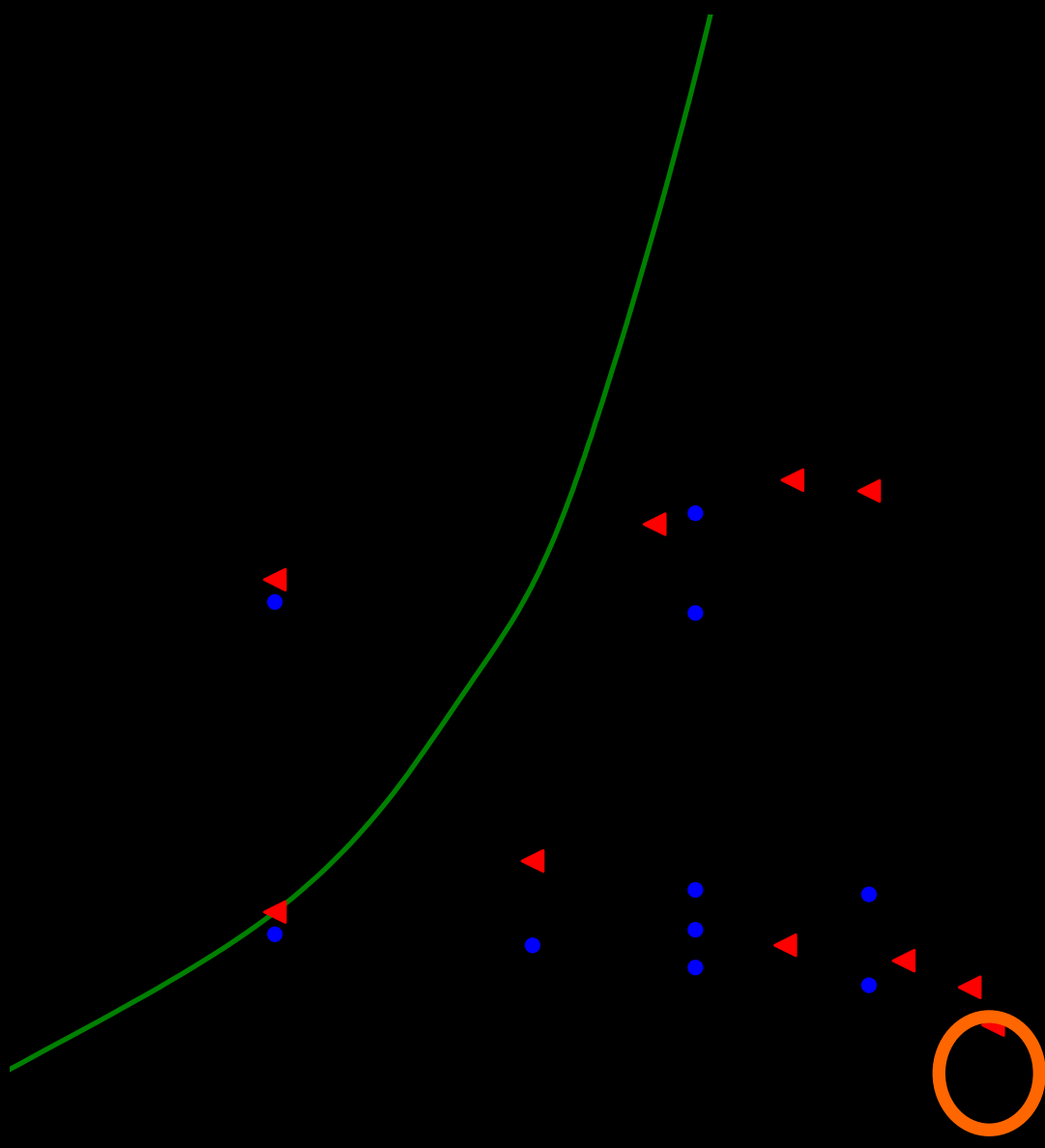
23.5 psia 100% O₂, 22.5 V

| Material | Wire Test Available Current at Ignition (A) | Scratch Test Available Current at Ignition (A) |
|------------------------|--|---|
| Generic cotton | 0.36 | 0.95 |
| Moleskin | 0.3 | 0.8 |
| UCN (shiny side) | 0.70 | 1.4 |
| Nylon/Lycra Comm Cap | 0.59 | 1.3 |
| Astronaut undergarment | 0.64 | 1.4 |
| LCVG spandex | 0.53 | 1.4 |
| LCVG tricot | 0.49 | 1.3 |

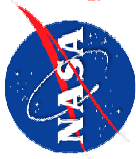




Moleskin



| | Material | Surface Characteristics |
|---|---|-------------------------|
| <div>Best</div> <div> <div></div> <div></div> </div> <div>Worst</div> | Interface cable Gore-Tex® sleeve | Smooth |
| | Urethane-coated nylon suit bladder (fabric side) | Smooth |
| | PVC | Smooth |
| | Interface cable polyurethane jacket | Smooth |
| | Urethane-coated nylon suit bladder (shiny side) | Smooth |
| | Astronaut longhandle undergarment | Fuzzy |
| | CCA cap spandex (nylon & Lycra® knit fabric) | Smooth |
| | LCVG garment (multifilament nylon / spandex knit 1106 treated with 3% TCHDE solution) | Smooth |
| | LCVG garment inner liner (nylon tricot treated with 3% TCHDE solution) | Smooth |
| | Cotton flocked Rucothane® glove bladder | Fuzzy |
| | TCU assembly (Capilene® – hollow fiber polyester treated with 3% TCHDE solution) (gray) | Fuzzy |
| | Kerlix dressing | Fuzzy |
| | Generic cotton | Fuzzy |
| | Moleskin | Fuzzy |



Conclusions

- Wire-break test is worst-case
- Fuzzy materials generally easier to ignite
- Current appears to have greater effect than voltage
- Controlling risk must include both
 - Physical isolation of easy to ignite materials
 - Limiting current and voltage